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TEST REPORT No : 05896-6012 Road

DATE OF ISSUE : 20 July 2023

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## BS EN 1793-2:2018

# **Road Traffic Noise Reducing Devices – Test Method for Determining the Acoustic Performance**

Part 2: Intrinsic Characteristics of Airborne Sound Insulation Under Diffuse Sound Field Conditions

Client:	Set 6 Ltd
Job Number:	05896
Test Sample:	Mute Acoustic Fence 80
Date(s) of Test:	17 May 2023

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Approved:.	

L Cambidge Specialist Acoustics Technician

D Wong-McSweeney Laboratory Manager

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#### **Client Details:**

**Manufacturer:** 

**Date Order Received:** 

Set 6 Ltd
Unit 5 Birch Court
Grosvenor Grange
Padgate
Warrington
WA1 4GD
Client
06 April 2023

## 1. <u>Test Samples</u>

The following sample was installed in the  $3600 \times 2800$  mm aperture of the transmission suite of the University of Salford Acoustic Test Laboratory. All information regarding the samples comes from laboratory measurements unless marked with "*cs*" or otherwise stated.

The test specimen was installed in accordance with clause 4 of BS EN 1793-2:2018 and conforming to BS EN ISO 10140-2:2021.

## **1.1. Description of Test Samples**

Test Reference:	05896-6012
Sample Reference cs:	Mute Acoustic Fence 80
Sample Description:	Road Noise Barrier

A road noise barrier was installed by the Client, on the receiving room side of the acoustic break in the test aperture. A vertical, prefabricated, H-section, metal post was fixed to the side of the test aperture, using L-brackets and screws. The post consisted of two channel assemblies, welded together back-to-back. The post was fitted with a D-section rubber seals on the receiving room side and screw-adjustable wedges on the source room side. On the side towards the side of the test aperture, the recess in the post was filled with a length of timber.

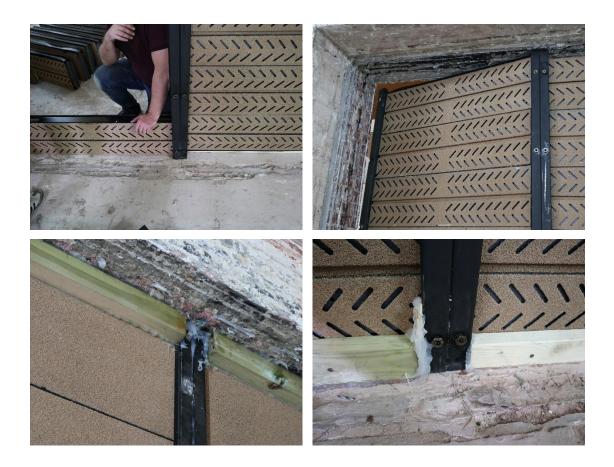




Nine acoustic panels were slotted into the post, with H-section rubber seals between each panel. Each panel was composed of metal rectangle box section planks filled with different types of plastic absorption. The source room face of each panel was pierced with holes, to expose the infill. Both source and receiving room faces were covered with a layer of rubber and cork granules. A single panel was measured to be 2400 mm  $\times$  297 mm  $\times$  75 mm, with a mass of 21.3 kg.



A second, intermediate post was fitted over the ends of the acoustic panels. A shorter, second set of acoustic panels and seals was slotted into the intermediate post, at a slight angle; before a third post was fitted over the end of the assembly, the other recess in this post was filled with a length of timber. The end of the barrier assembly was then moved into its correct position in the test aperture and fixed in place, using L-brackets and screws.



Lengths of timber (screwed to the top panel) were added to close the gap between the barrier and the top of the test aperture, on both source room and receiving room faces. More lengths of timber were screwed to the lowest panel, on the source room face only, to close the gap between the barrier and the base of the test aperture.



Silicone sealant was used to seal the perimeter of the barrier and the centre seams of the posts, on both source room and receiving room faces. More silicone sealant was used

to fix small pieces of wood over holes in the posts, where wedge adjustment screws were not fitted.

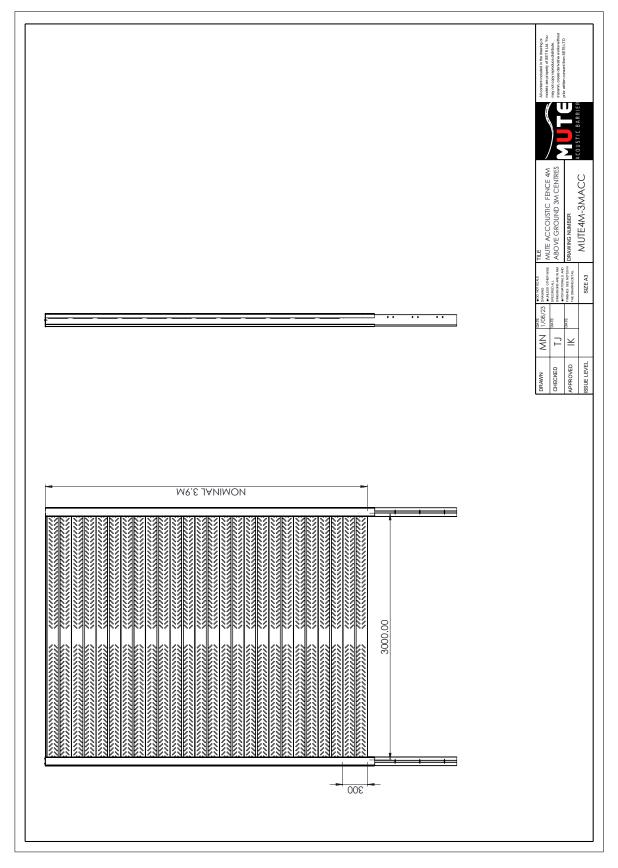


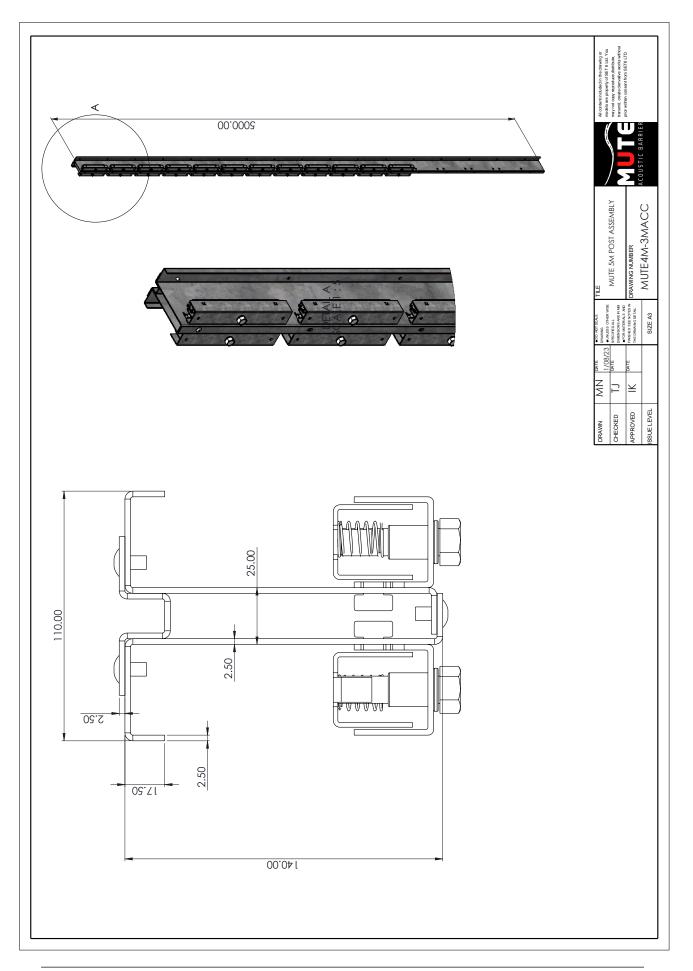
Mass per unit area:	$29.9 \text{ kg/m}^2$
Thickness:	75 mm (plank thickness)

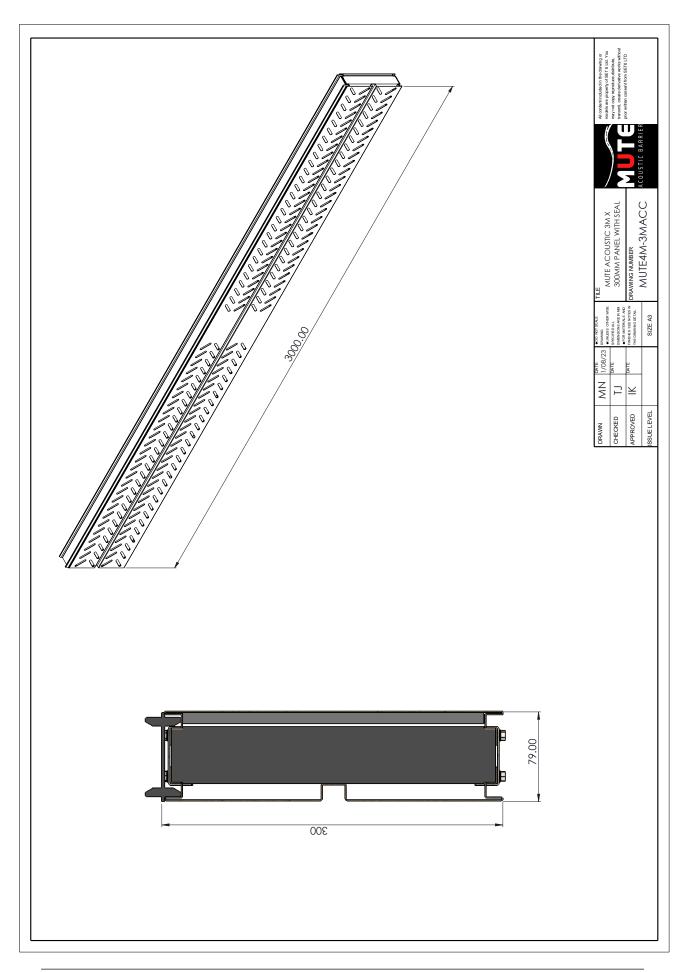
#### **1.2.** Sectional Drawings

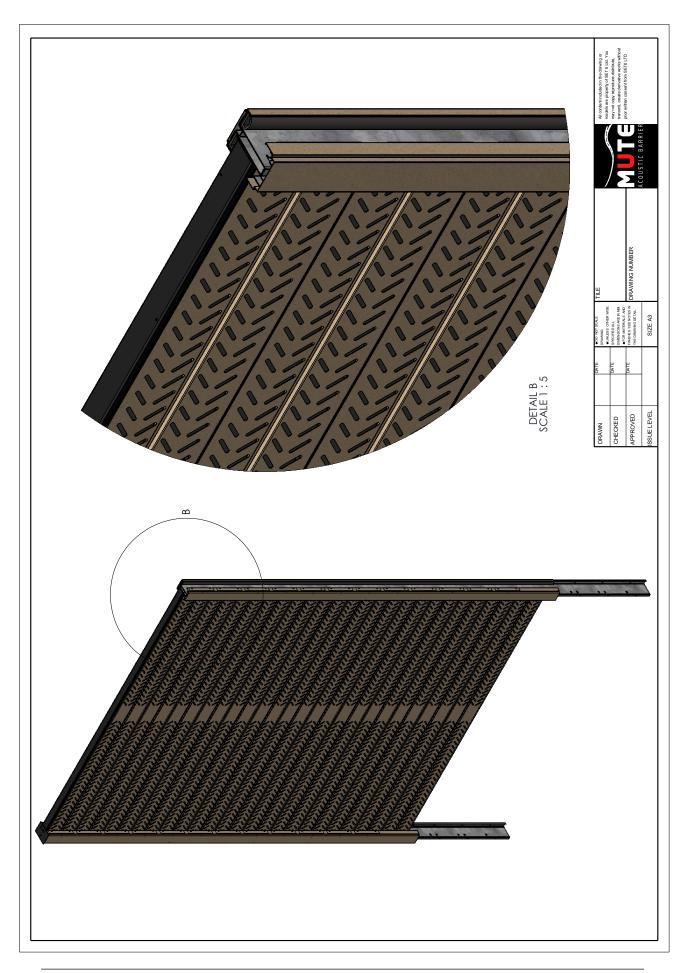
Sectional drawings, as provided by the client, can be found below.

## Test Reference: 05896-6012









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## 2. <u>Description of Test Procedure</u>

The test procedure adopted follows that detailed in BS EN 1793-2:2018, conforming to BS EN ISO 10140-2: 2021, "Acoustics – Laboratory measurements of sound insulation of building elements; Part 2: Measurement of airborne sound insulation".

The measurements are performed in the large transmission suite at the University of Salford. The suite comprises two structurally isolated reverberant rooms with a test opening between them in which the test specimen is inserted. The vertical sides of the test aperture are made from dense brick, whilst the soffit is made from reinforced concrete. Both rooms have been designed with hard surfaces and non-parallel walls. The smaller source room has 4 plywood diffusers and the larger receiving room has 18 plywood diffusers, to increase the diffusivity of the sound field in these areas.

The test involves producing a known sound field in the source room and measuring the resultant sound level difference between the source room and the receiving room with the specimen installed in the test aperture. This level difference is then corrected so as to take into account the equivalent absorption area of the receiving room.

The Sound Reduction Index, R (dB), is defined in BS EN ISO 10140-2:2021 as:

$$R = L_1 - L_2 + 10 \log_{10} \frac{S}{A} \tag{1}$$

where:

 $L_1$  is the average sound pressure level in the source room (dB)  $L_2$  is the average sound pressure level in the receiving room (dB) *S* is the area of the test specimen (m<sup>2</sup>) *A* is the equivalent absorption area of the receiving room (m<sup>2</sup>)

#### 2.1. Generation of Sound Field in the Source Room

Wide band, random noise from the generator in the real time analyser was amplified and reproduced in the source room using alternately one of three fixed loudspeaker systems, (**La** and **Lb** and **Lc**). Omni-directional loudspeakers were used. The output of the generator was set with the intention that the sound pressure level in the receiving room was at least 15 dB higher than the background level in any frequency band. The loudspeakers were positioned in the corners of the room and at such a distance from the test specimen that the direct radiation upon it was not dominant.

### 2.2. Frequency Range of Measurements

The sound pressure levels were measured using one-third octave band filters. Measurements covered all the one-third octave bands having centre frequencies in the range from 50 Hz to 5000Hz.

### 2.3. Measurement of Sound Pressure Levels

Sound pressure levels were measured simultaneously in the source and receiving rooms using loudspeaker **La** as the sound source. Measurements were recorded at 6 fixed microphone positions in each room, using an averaging time of 16 seconds and the average level in each room was calculated on an energy basis in each one-third octave frequency band. The procedure was then repeated with loudspeakers **Lb** and **Lc** as the sound source. The overall average level difference in each frequency band was then calculated as the arithmetic average of the two sets of results.

For each set of microphone/loudspeaker positions, the distances separating microphones from other microphones, room boundaries and diffusers, were greater than 0.7 m and the distances separating microphones from the sound source and the test specimen were greater than 1.0 m.

#### 2.4. Measurement and Evaluation of the Equivalent Absorption Areas

The correction term of equation (1) containing the equivalent absorption area, *A*, was evaluated from the reverberation time and calculated using Sabine's formula:

$$A = \frac{0.16 V}{T} \tag{2}$$

where:

V is the volume of the receiving room  $(m^3)$ 

T is the reverberation time (s)

The reverberation time of the receiving room was measured using a decay technique. The decays were produced by exciting the room with wide band random noise and stopping the excitation once the room became saturated. The resulting decaying sound field was monitored at 6 fixed microphone positions using a one-third octave band real time analyser. The sound spectrum was sampled and stored in memory. Five decays were measured at each microphone position and averaged. The time taken for the sound to decay by a given amount was measured and then extrapolated to determine the reverberation time. The measurements were repeated using an alternative sound source. The results from each set of positions were averaged (ie 60 reverberation decays at each frequency).

# 3. <u>Equipment</u>

Equipment	Laboratory Equipment Record No.
$2\times$ Norwegian Electronics 1/3 octave band real time analyser type 850 with in-built random noise generator	RTA3-01 to 12
Quad 510 power amplifier	PA7
Norsonic Sound Calibrator type 1251	C8
$2 \times Norsonic Dodecahedron Loudspeakers$	LS10-LS11
$3 \times Norsonic Dodecahedron Loudspeakers$	LS12-LS14
$3 \times$ Bruel & Kjaer random incidence condenser microphones type 4166 in the source room	M2-M4
$3\times G.R.A.S.$ random incidence condenser microphones type 40AP in the source room	M21, M22, M30
$2 \times$ Bruel &Kjaer random incidence condenser microphone type 4166 in the receiving room	M9, M18
$4\times G.R.A.S.$ random incidence condenser microphones type 40AP in the receiving room	M20, M31, M19, M32
Environmental sensor data logger, hygrometers and barometer	HL1, HG1, HG2, BM3
Toshiba TECRA R850 119 laptop computer and related peripheral equipment (network switch, printer, monitor etc.)	RTA3-00
Yamaha GQ1031BII graphic equalizer	GEQ1

## 4. <u>Results</u>

Source room volume:	$136 \text{ m}^3$
Receiving room volume:	222 m <sup>3</sup>
Sample sizes:	$3600 \text{ mm} \times 2800 \text{ mm}$

The sound reduction indices at one-third octave band intervals, R, are given in the tables overleaf.

Also given in the attached tables is the single number rating  $DL_R$ . This is calculated in from the one third octave sound reduction indices in accordance with BS EN 1793-2:2018 and uses the Normalised Traffic Noise Spectrum described in BS EN 1793-3:1998. This evaluation is based on laboratory measurement results obtained by an engineering method.

The results here presented relate only to the items tested and described in this report.

## BS EN 1793-2 : 2018, Intrinsic Characteristics of Airborne Sound Insulation

Client: Set 6 L	td			Pro	duct ID:	Mute Acou	istic Fence 8	30	
Mounted by: Client									
Sample Size: 10.08	m²			Tes	st Room ID	: Acoustic T	ransmission	Suite	
Manufacturer: Client				Dat	te of Test:	17 May 20	23		
Description: Road N	loise Barrier								
Source Room Volume:		136	m <sup>3</sup>	Ambi	ent Pressu	re:		102.5 kł	Pa
Source Room Temperatur	e:	20.2	°C	Meas	ured Mass	per unit area	:	29.9 kg	g/m²
Source Room Relative Hu	midity:	44.6	%	Curin	g Time:			Not Applic	able
Receiving Room Volume:		222	m <sup>3</sup>						
Receiving Room Tempera	ture:	20.6	°C						
Receiving Room Relative	Humidity:	44.2	%		R				
				-	ĸ				
	$\uparrow$	<sup>60</sup> T							
Frequency R	- -								
f <sup>1</sup> ⁄₃ octave	[dB								
[Hz] [dB]	dex								
50 22.0	<u> </u>	50							
63 22.4	Ictio								
80 19.9	tedu								
100 19.5	Sound Reduction Index [dB]								
125 19.9	sour	10							
160 17.0 200 17.9	(U	40						/	
250 17.9									
315 21.4									
400 22.0									
500 22.6		30					/		
630 23.5									
800 24.9									
1000 27.1									
1250 31.3		ŀ							
1600 34.5		20		~					
2000 36.9									
2500 38.8									
3150 40.1									
4000 41.4		10							
5000 43.8									
		。 							
		0 +	63	125	250	500	1000	2000	4000
Pating according to PS EN 4	703-2						Freque	ncy, f [Hz]	$\rightarrow$
Rating according to BS EN 1									
DL <sub>R</sub> =	25 dB								
Evaluation ba	sed on laboratory	measure	ement resul	ts obtained in o	one-third-octa	ive bands by an	engineering n	nethod.	
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